

EXACT Analysis

Exact Analysis of the Carburettor :- (with Compressibility of air into consideration)

Section A-A → Point 1 - (At the inlet of the carburettor)
 Section B-B → Point 2 → (Venturi Throat)

⇒ Applying Steady flow energy Eqⁿ to section A-A & B-B

① ⇒ Assuming unit mass flow of air ($m = 1 \text{ kg}$)

$$q_h - w = (h_2 - h_1) + \frac{1}{2} (c_2^2 - c_1^2)$$

Where,

② ⇒ Assuming an adiabatic flow $q_h = 0$, $w = 0$

③ ⇒ Assuming $c_1 \approx 0$

$$c_2 = \sqrt{2(h_1 - h_2)} = \sqrt{2\Delta h}$$

Δh → Adiabatic Enthalpy change

④ ⇒ Assuming air to behave as ideal gas,
 $h = c_p T$

$$c_2 = \sqrt{2c_p(T_1 - T_2)}$$

⑤ ⇒ Assuming the flow to be Isentropic

$$c_2 = \sqrt{2c_p T_1 \left[1 - \left(\frac{P_2}{P_1} \right)^{\frac{\gamma-1}{\gamma}} \right]}$$

C_{da} → Co-eff of discharge for venturi (contraction of stream + η)

Z - Height of the nozzle exit above the level of fuel in the float chamber

Mass Flow-rate ^{of air} at Venturi Throat:

$$m_a = \frac{A_2 P_1}{R \sqrt{T_1}} \sqrt{2c_p \left[\left(\frac{P_2}{P_1} \right)^{\frac{2}{\gamma}} - \left(\frac{P_2}{P_1} \right)^{\frac{\gamma+1}{\gamma}} \right]}$$

From

$$m = \rho_1 A_1 c_1 = \rho_2 A_2 c_2$$

$$m_{a \text{ Actual}} = C_{da} \times m_{a \text{ Th}}$$

$$\frac{P_1}{\rho_f} - \frac{P_2}{\rho_f} = \frac{c_f^2}{2} + gz$$

$$c_f = \sqrt{2 \left[\frac{P_1 - P_2}{\rho_f} - gz \right]}$$

$$m_{f \text{ Th}} = \rho_f A_f c_f = A_f \sqrt{2\rho_f (P_1 - P_2 - gZ\rho_f)}$$

Applying Bernoulli's Thⁿ & fuel is incompressible.